



SATURN ELECTRONICS
CORPORATION

MCPCBs for LED Applications

Thermal Management Material Specifications





SATURN ELECTRONICS
CORPORATION

Purpose of the Webinar

Defining your needs

To break down your needs for thermal management materials, specifically metal core printed circuit board (MCPCB), in LED Applications by *technical requirements* in order to make more effective callouts.

Controlling the process

The end result should be shorter lead times, lower cost, and more reliable product.

Non-browning soldermasks

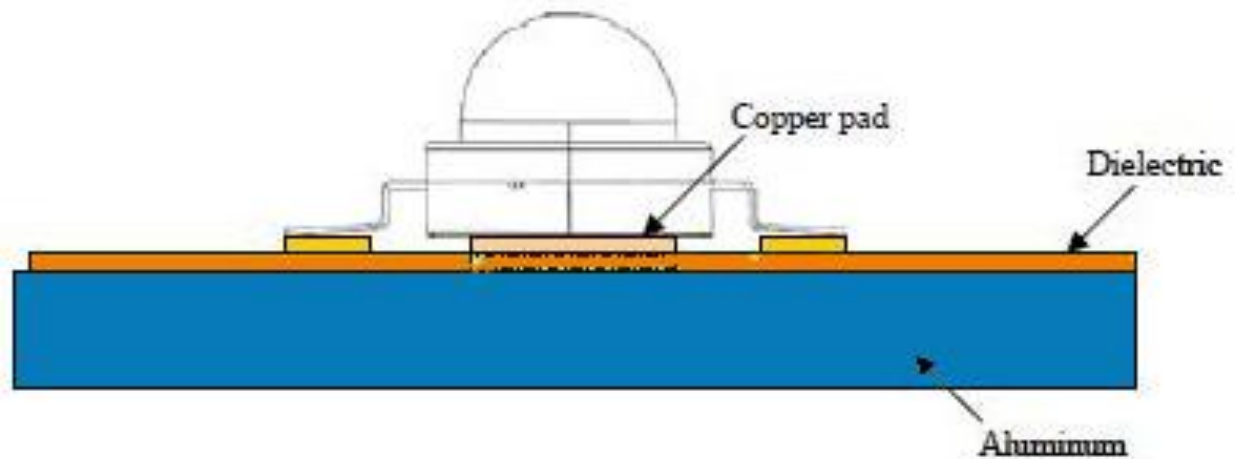
Introduce new non-browning white LED soldermasks.



Metal Core Boards

Definition

The MCPCB commonly consists of a metal core layer (typically aluminum or copper), a continuous dielectric layer and a copper circuit layer.

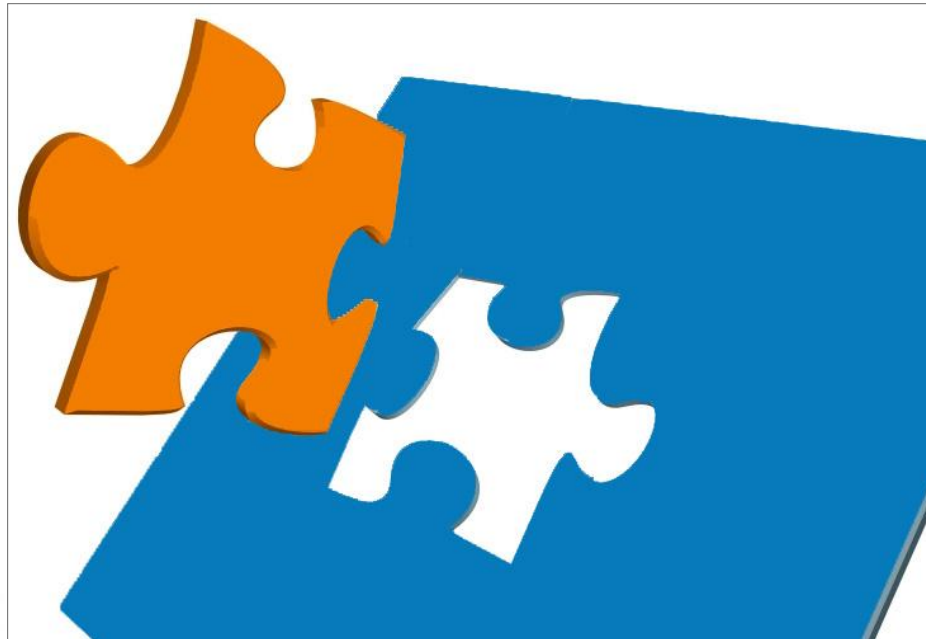




SATURN ELECTRONICS
CORPORATION

Part One

Specifying Materials for LED Applications





SATURN ELECTRONICS
CORPORATION

Survey Question

How do you specify materials in MCPCB LED applications?

- a) Company Name and/or Part Number (e.g. Bergquist, Laird, DuPont, etc.)
- b) Thickness of dielectric
- c) T_g or T_d
- d) "Metal Core"
- e) Insulation Resistance & Thermal Conductivity Values





SATURN ELECTRONICS
CORPORATION

Survey Answer

How do you specify materials in metal core LED applications?

a) Company Name and/or Part Number (e.g. Bergquist, Laird, DuPont, etc.)

Comment

Specifying by brand name locks you into a particular product produced by a particular manufacturer.

Risks Include:

- Locked into pricing
- Subject to lead times
- Preventing new materials from being used on your product



Survey Answer

How do you specify materials in metal core LED applications?

- b) Thickness of dielectric,
- c) T_g ,
- d) T_d

Specifying only these items may not fully address your needs.

- Does not address thermal conductivity
- Does not address electrical insulation resistance
- Does not address type of dielectric



SATURN ELECTRONICS
CORPORATION

Answer

How do you specify materials in metal core LED applications?

e) “Metal Core”

Comment:

Specifying “metal core” does address anything whatsoever.



Answer

How do you specify materials in metal core LED applications?

f) Insulation Resistance & Thermal Conductivity Values

Comment:

You are a rock star! This is the whole point of our webinar.





SATURN ELECTRONICS
CORPORATION

Consider *your needs* when bringing the bare board into the equation





SATURN ELECTRONICS
CORPORATION

Survey Question

What Are Your Needs When Selecting Materials? (Choose all that apply)

- a) Transfer heat (Thermal Conductivity)
- b) Prevent short circuiting to base metal core (Electrical Insulation Resistance)
- c) Thickness of dielectric
- d) Brand name of the material?





Cost Drivers For MCPCBs

Dielectric Substrate

The # 1 cost component of the MCPCB is the dielectric substrate between the copper traces and the metal heatsink / core.

Definition

An insulating medium which occupies the region between two conductors. In this case, the copper circuits and the metal core heat sink.



Cost Drivers For MCPCBs (cont.)

Introducing competition

The most effective way to reduce cost of dielectric is to introduce competition:

- Laird
- Bergquist
- Dupont
- Uniplus
- Iteq
- Insulectro
- Plus future innovators



SATURN ELECTRONICS
CORPORATION

Definition and Applications

Thermal Transfer

Product Application

Electrical Insulation

Product Reliability



SATURN ELECTRONICS
CORPORATION

Purpose #1

Transfer Heat

Common Callouts include Thermal Impedance / Resistance ($^{\circ}\text{C in}^2/\text{W}$) and Thermal Conductivity / ($^{\circ}\text{W}/\text{m-K}$).



SATURN ELECTRONICS
CORPORATION

Why Kapton® / Polyimide?

Heat Resistance

Stability

Flexibility

Dielectric Properties

Density/Weight



CooLam™ MCPCB (metal core PCB) Offers:

- Very Low Thermal Impedance
- Excellent Reliability Performance
- Excellent Durability and Stability at High Temperature
- Uniform Thermal, Mechanical & Electrical Properties Under Environmental Stress
- Lead Free Solder and Wirebond Process Compatibility
- Halogen Free
- Meets UL 94 V-0
- Construction Variations to Meet Thermal Management Needs
- 3D Shapes





Thermal Measurement

Characterize the Thermal Performance of Materials

Objective:

Measuring thermal performance per ASTM D5470.

Equipment:

- 1) Steady State “Thermal Interface Material Tester” (TIM)
(Analysis Tech. Inc.)

Factors to Consider:

- 1) Reducing contact resistance between sample and test unit
- 2) Repeatability of measured values
- 3) Identify any equipment and/or material limitations



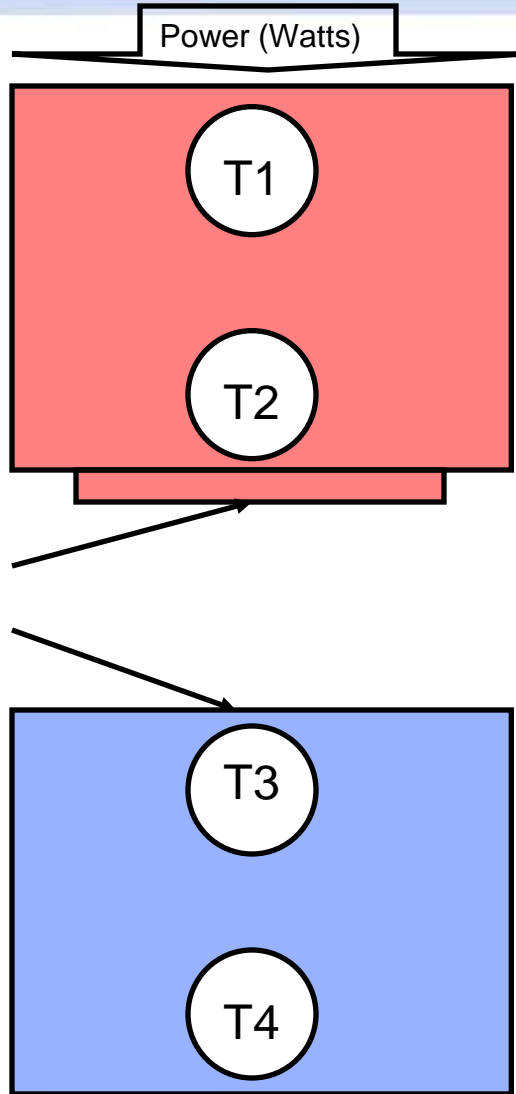
Basic Principles of ASTM D5470

What is Thermal Resistance ?

Thermal Resistance (R_{th}) is defined as the difference in temperature between two closed isothermal surfaces divided by the total heat flow between them.

$$R_{th} = (T_{(A)} - T_{(B)}) \div \text{Power}$$

$$\frac{\Delta^{\circ}\text{C}}{\text{Watt (V*I)}}$$



Heat Source

(surface A)

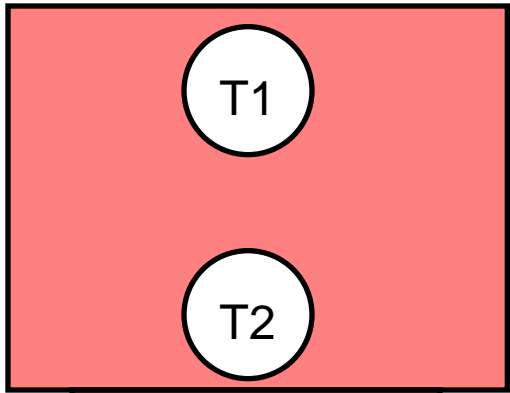
(surface B)

Heat Sink

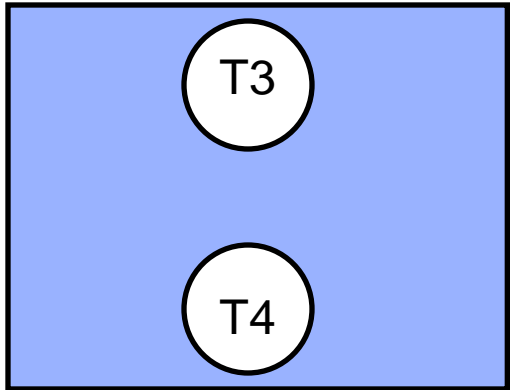
* Present system does a good job of accounting for all heat and monitoring temperature but nothing is perfect.



Power (Watts)



Test Sample



Output from TIM unit:

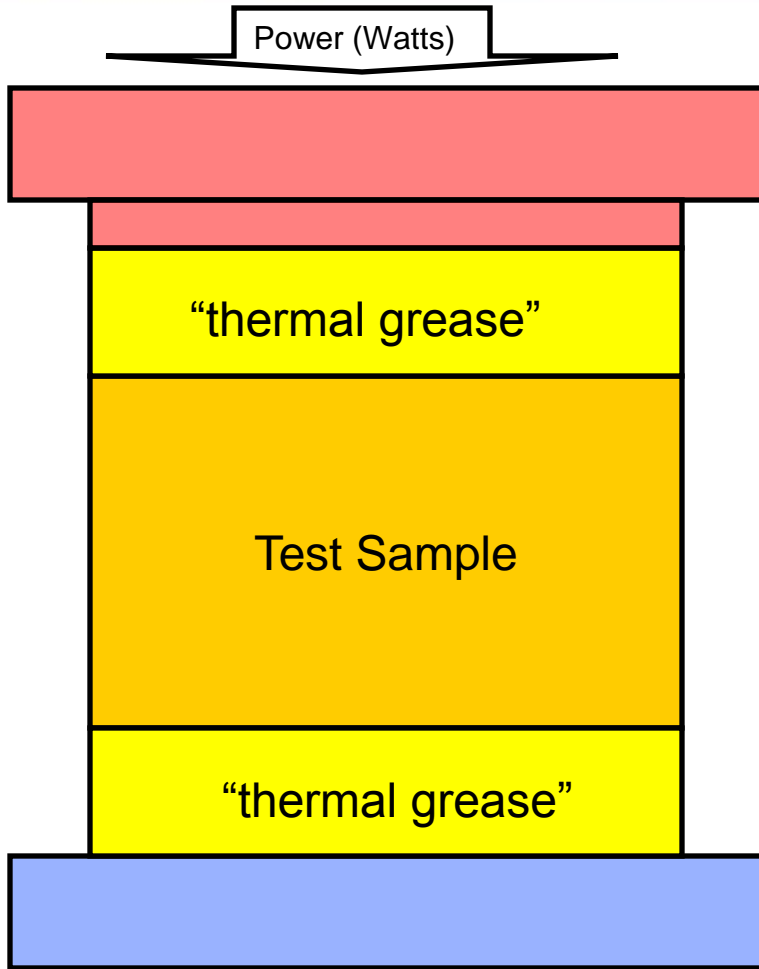
Thermal Resistance (R_{th}): $\frac{\Delta^{\circ}\text{C}}{\text{Watt}}$
 = (Δ Temp. \div power)



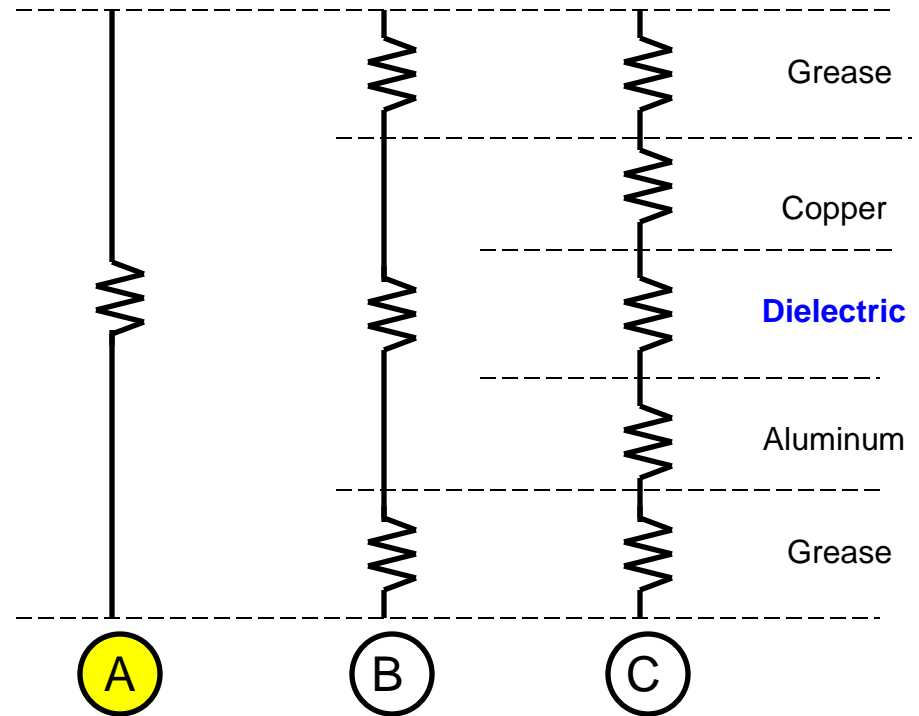
Thermal Impedance (R_{thI}): $\frac{^{\circ}\text{C} - \text{in}^2}{\text{Watt}}$
 = (Thermal Resistance) x area (of test sample)

and

Thermal Conductivity: $\frac{\text{Watt}}{\text{m} - ^{\circ}\text{C}}$
 = thickness (material) \div thermal impedance



- Total Thermal Resistance ($R_{th\ total}$) is the sum of components and its thermal resistance value.

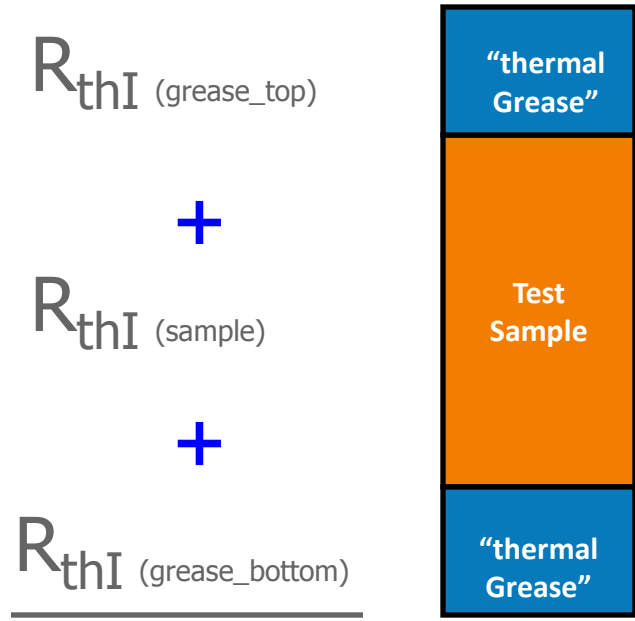


ASTM D5470 Thermal Measurement Technique



ASTM D5470 Thermal Measurement Technique

Measured Thermal Impedance (C-in²/Watt):



$R_{thI (grease_top)}$

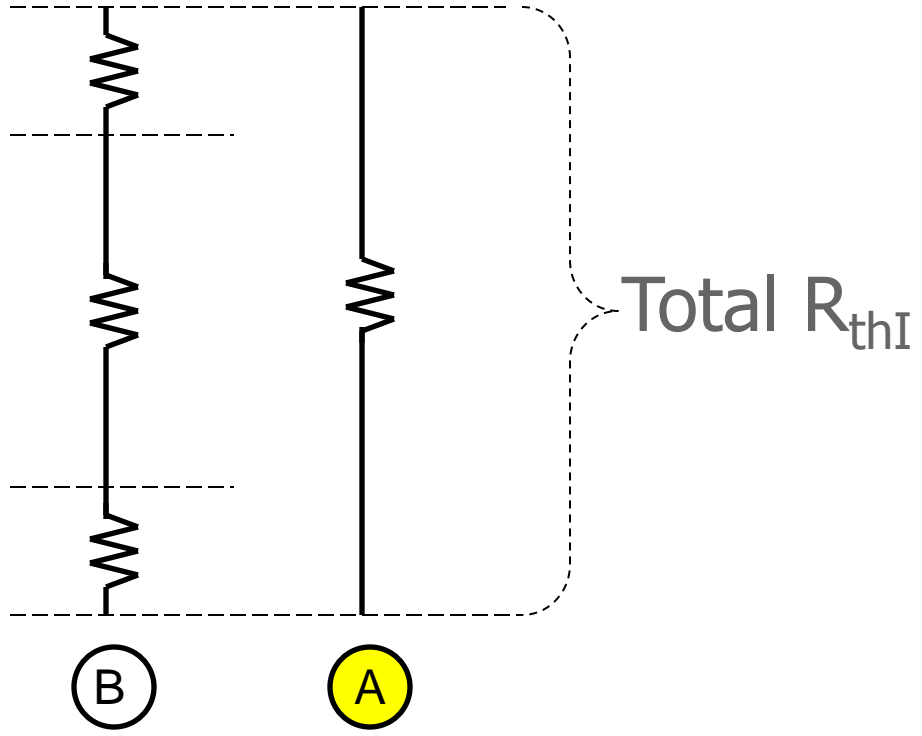
+

$R_{thI (sample)}$

+

$R_{thI (grease_bottom)}$

Total R_{thI}



$$R_{thI (sample)} = \text{Total } R_{thI} - (R_{thI (grease_top)} + R_{thI (grease-bottom)})$$



Thermal Impedance

Electronics industry defines thermal impedance as the following:

$$\textit{impedance}_{thermal} = \frac{\textit{thickness}}{k}$$

This does **not** include an area through which the heat flows!

Thermal Impedance

$$I = \frac{t_{Diel}}{k_{Diel}}$$

Units:

$$I \rightarrow \frac{m}{\frac{W}{mK}} = \frac{m^2 K}{W}$$

Thermal Resistance

$$R = \frac{t_{Diel}}{k_{Diel} A}$$

Units:

$$R \rightarrow \frac{m}{\frac{W}{mK} m^2} = \frac{K}{W}$$



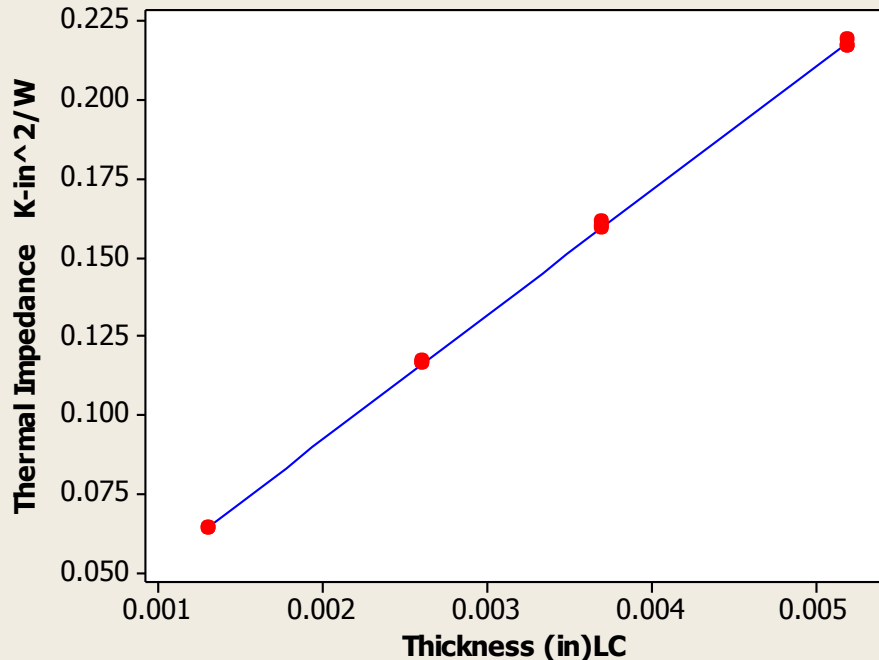
Thermal Impedance

Calculating the thermal conductivity of a material

Plot Ra vs. thickness from TIM tester

1/k =thermal conductivity k = is the slope of the line

Fitted Line Plot
K-in²/W = 0.01366 + 39.35 Thickness (in)



S	0.0010461
R-Sq	100.0%
R-Sq(adj)	100.0%

Thermal Conductivity LG:
0.25 W/M-K

= 1.0 in / 39.35 K-in²/W
 = .006394 W/in-K x 39.4
 in/M (convert to metric)
 = **1.0 W/M-K**

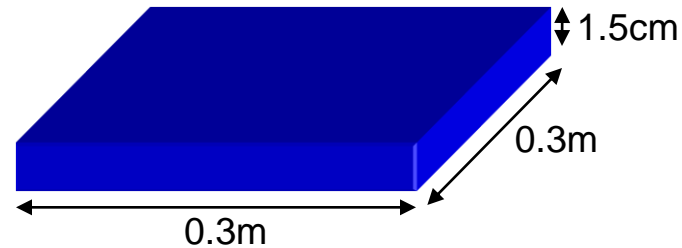


Example problems

What is the thermal resistance through the thickness of a 0.3 meter by 0.3 meter piece of stainless steel that is 1.5 cm thick? Assume the thermal conductivity of stainless steel is 15 W/mK.

$$k=15 \text{ W/mK}$$

$$R = \frac{t}{kA}$$



$$R = \frac{t}{kA} = \frac{0.015m}{(15W/mK)(0.3m)(0.3m)}$$

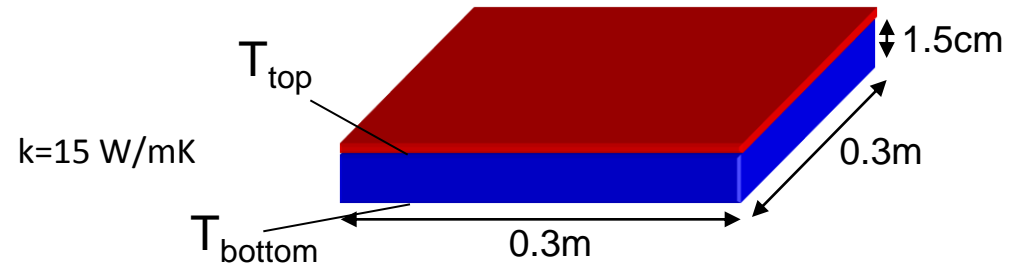
$$R = 0.011 K/W$$



Example Problems

This same piece of stainless steel now has a heater attached to one side that generates 100 Watts of heat into the plate.

If the bottom of the plate measures 45°C (318K), what is the temperature of the top side of the plate?



$$q = \frac{(T_{top} - T_{bottom})}{R_{thermal}} \rightarrow (T_{top} - T_{bottom}) = q \cdot R_{thermal}$$

$$T_{top} = q \cdot R_{thermal} + T_{bottom}$$

$$T_{top} = 100W \cdot 0.011K/W + 318K$$

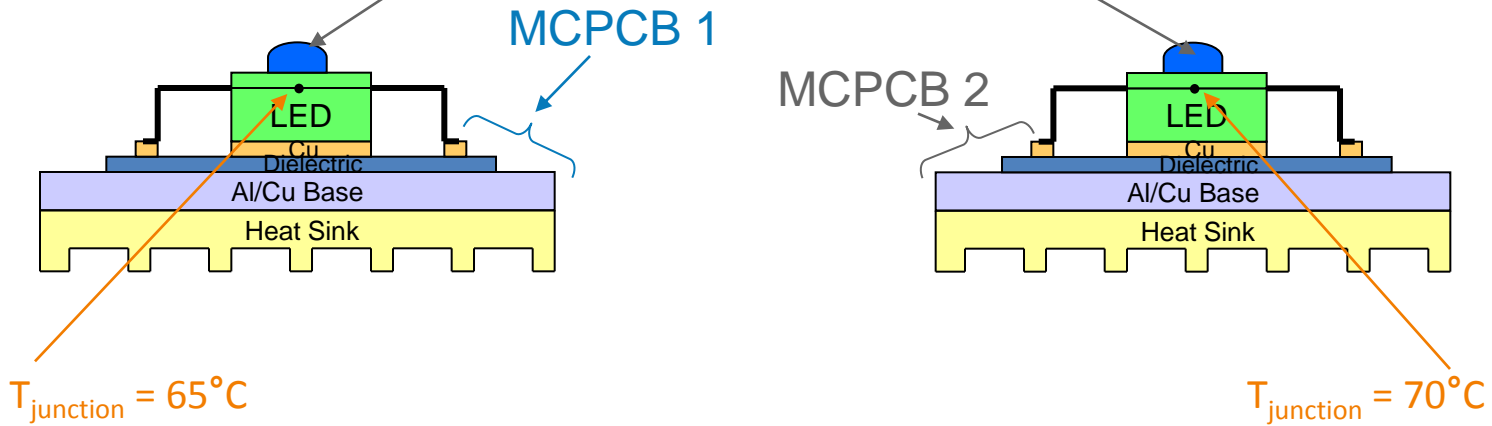
$$T_{top} = 319.1K = 46.1^\circ C$$



Basic Question

Room Temp = 30°C

Same LED and power input



WHY???

Heat Transfer





SATURN ELECTRONICS
CORPORATION

Thermal Management for LED Applications

What is the role of the PCB?

Presented by Clemens Lasance

Clemens is a former Principal Scientist Emeritus with Philips Research, the Netherlands, with a 30 year + focus on thermal management of electronic systems.

He is now a consultant for *Somelikeit Cool*, contact info: lasance@onsnet.nu



SATURN ELECTRONICS
CORPORATION

Motivation

Providing the right information the first time

The goal is to provide the LED application engineer with the right information to select the most optimal MCPCB from a thermal point of view. Thus, ensuring the best decision is made for a specific application in regards to thermal performance and cost.





Main Goal of Thermal Management

The Calculation of application-specific junction temperatures

Reasons / Key Issues

- Lifetime
- Color point
- Efficiency

All these key issues are significantly dependent on the junction temperature.



Basics of Heat Transfer

Fundamentals of Critical Temperature Calculation

Determining critical temperatures is contingent upon a critical understanding of:

- The electrothermal analogue
- Thermal conductivity k
- Heat transfer coefficient h
- Thermal resistance R_{th}



Electro-Thermal Analogue

$$\Delta T = q * R_{th}$$



$$\Delta V = I * R$$

Temperature drop (°C)



Voltage drop (V)

Power dissipation (W)



Current (A)

Heat flux (W/m²)



Current density (A/m²)

Thermal resistance (K/W)

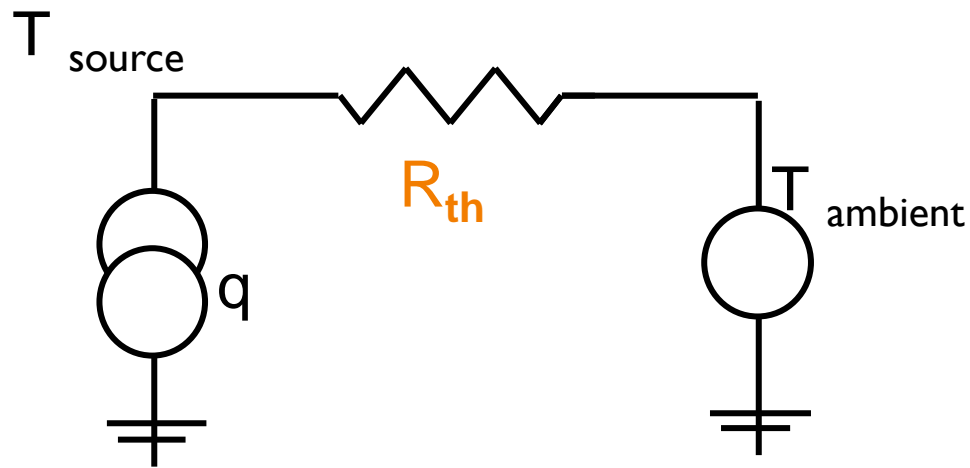


Resistance (Ohm)



Electro-Thermal Analogue

A heat transfer path can be described by an electrical network



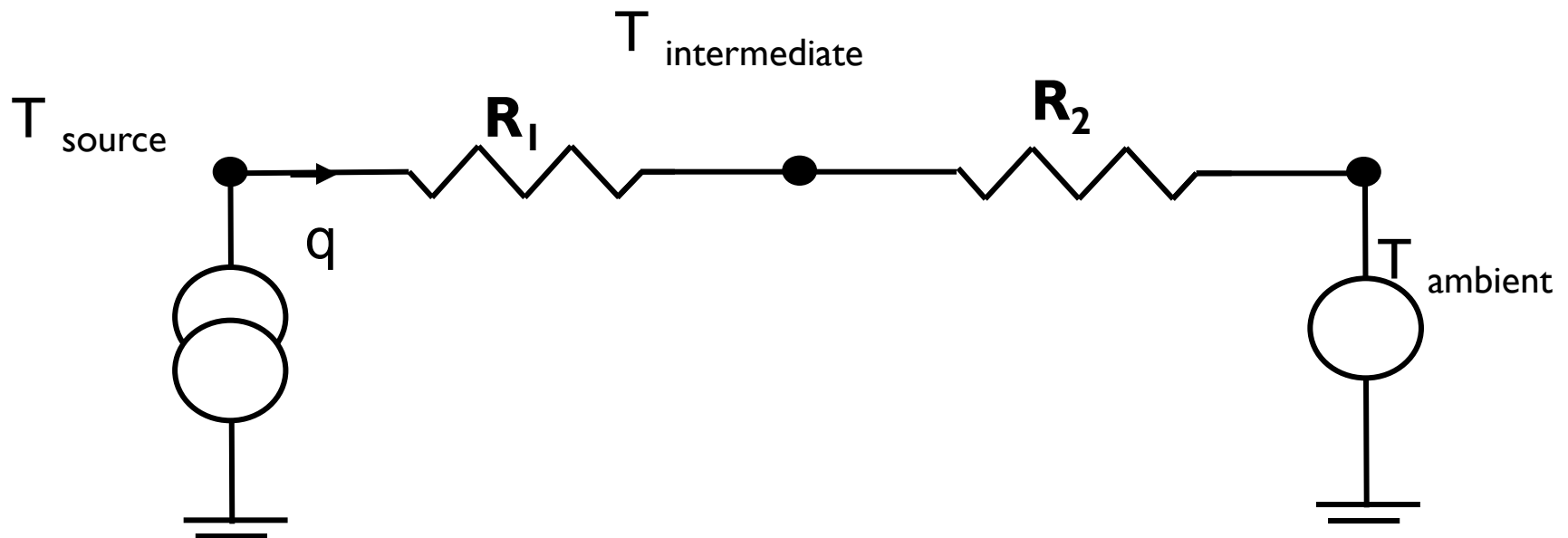
$$\Delta T = T_{\text{source}} - T_{\text{ambient}}$$

R_{th} (K/W) = thermal resistance



Series Circuit

Example for two resistances in series



$$\Delta T = T_{\text{source}} - T_{\text{ambient}} = q * R_{\text{total}}$$

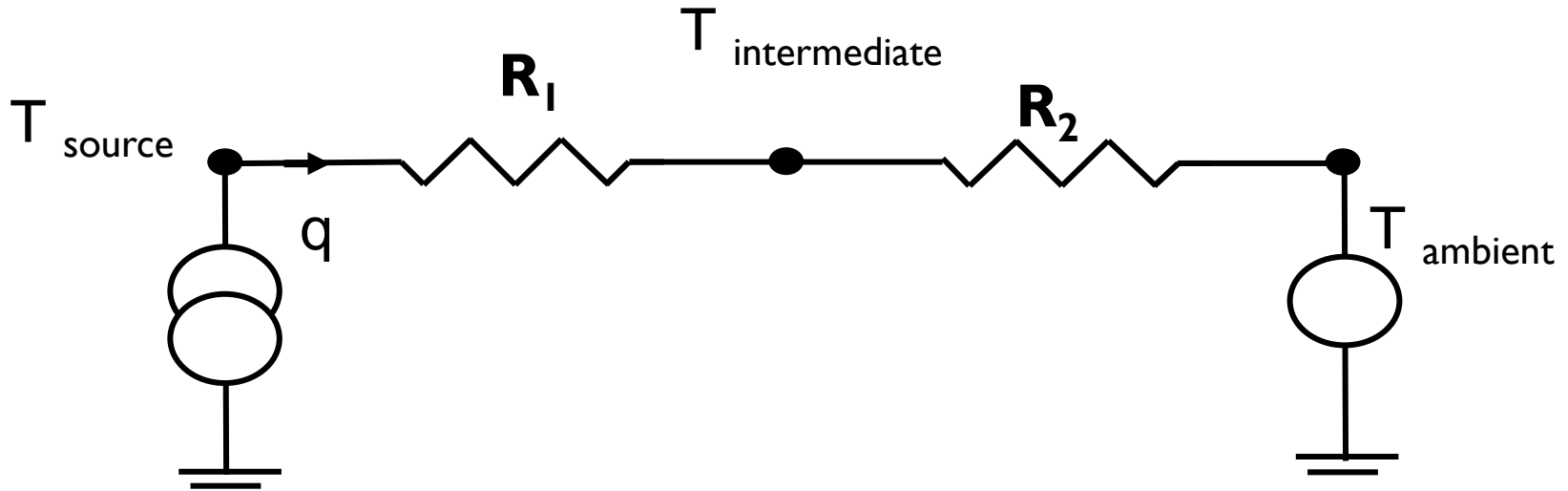
$$R_{\text{total}} = R_1 + R_2$$



SATURN ELECTRONICS
CORPORATION

Consequence of Series Circuit

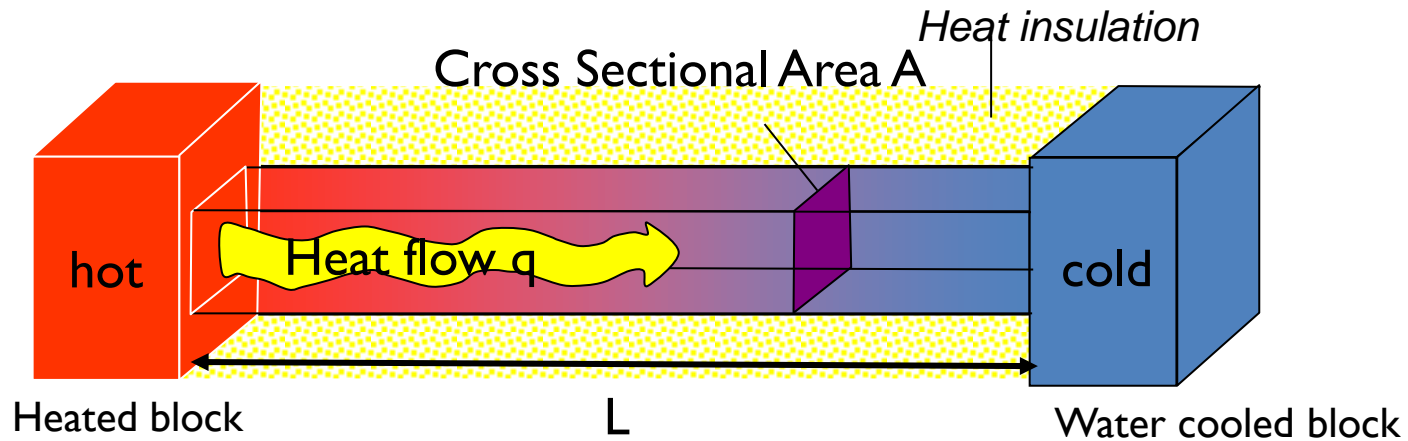
Often only the largest R is relevant!



Designer's job: find the largest resistance!



Thermal Conductivity: Fourier's Experiment (1822)



Result of Fourier's experiment:

- $q \sim \Delta T = T_{\text{hot}} - T_{\text{cold}}$
- $q \sim A = \text{cross-sectional area}$
- $q \sim L^{-1}$

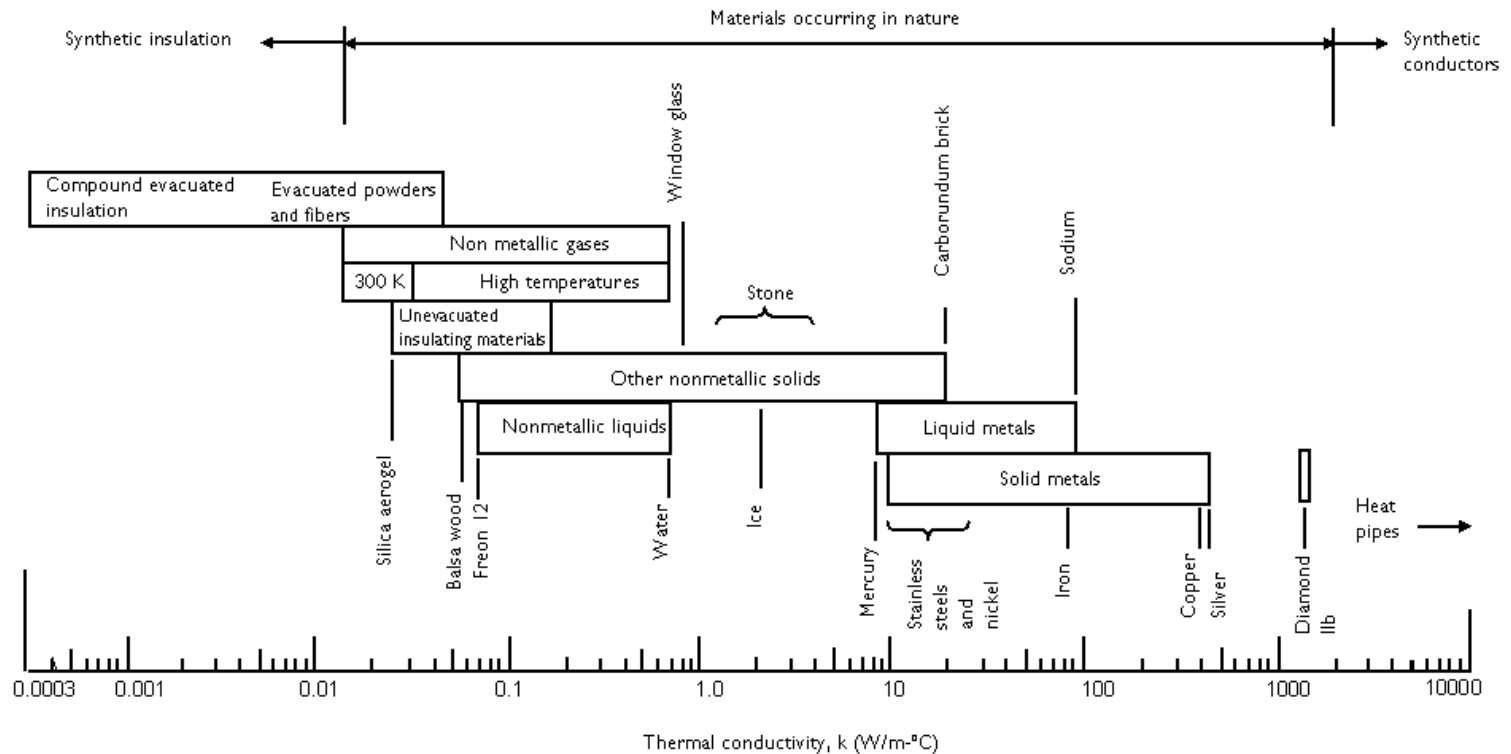


$$q = k \cdot \frac{A}{L} \cdot \Delta T$$

The proportionality constant k is called the 'thermal conductivity'



Typical Thermal Conductivity Values



Approximate ranges of thermal conductivity for various substances
(All values are in the neighborhood of room temperature unless noted)



The Heat Transfer Coefficient h

The heat transfer from a solid wall into a fluid (air, water) is called convection, and to first order this heat transfer is proportional to the area and the temperature difference between the wall and the fluid:

$$q = h \cdot A \cdot \Delta T$$

The proportionality constant h is called the
'heat transfer coefficient'

Typical values:

Natural convection: 10 W/m²K

Forced convection: 50 W/m²K



Practice

Suppose a Designer needs 5W to reach a required light output

What procedure is most optimal?

Information required for first order guess:

- Maximum junction temperature: e.g. 120 °C
- Maximum ambient temperature: e.g. 40 °C
- An estimation of all thermal resistances in the total heat transfer path

$$q = \frac{\Delta T}{R_{th-total}}$$



Practice (2)

Next steps

- Check if required power is manageable by suitable heat sinks & convection
- Check which thermal resistances are dominant
 - Then focus on them to reduce the total thermal resistance
- Final step should always be a detailed analysis
 - Recall that often we don't talk one-dimensional heat transfer but heat spreading, which is a rather complicated issue
 - For more information please see *Heat Spreading, Not a Trivial Problem* in the May 2008 issue of **ElectronicsCooling**



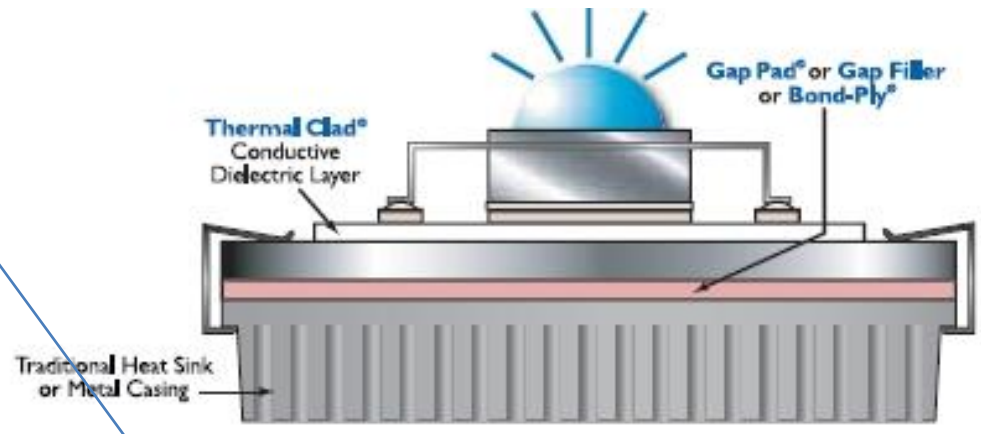
Practical Example

$$q = k \cdot \frac{A}{L} \cdot \Delta T$$

$$R_{th} = \frac{L}{k \cdot A}$$

$$q = h \cdot A \cdot \Delta T$$

$$R_{th} = \frac{1}{h \cdot A}$$



Relevant thermal resistances, assume 1 cm² PCB

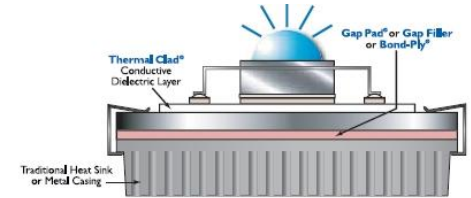
	K/W	
R _{th} -LED	16	Luxeon Rebel
R _{th} -MCPCB	0.5	t = 100 μm, k = 2 W/mK
R _{th} -TIM	1	t = 100 μm, k = 1 W/mK
R _{th} -heatsink	50	A = 20 cm ² , h = 10 W/m ² K
R _{th} -heatsink	2	A = 100 cm ² , h = 50 W/m ² K
R _{th} -heatsink	1	A = 1 cm ² , h = 10000 W/m ² K



Practical Example

We need 5W for our light output

Can we find a suitable heat sink?



We have:

$$T_{\text{junction}} = 120 \text{ }^{\circ}\text{C}$$

$$T_{\text{ambient}} = 40 \text{ }^{\circ}\text{C}$$

$$R_{\text{th-LED}} + R_{\text{th-MCPCB}} + R_{\text{th-TIM}} = 17.5 \text{ K/W}; R_{\text{th-heatsink}} = ?$$

Can we dissipate 5W? No way:

$$q = 80 / (17.5 + R_{\text{th-heatsink}})$$

$$q = \frac{\Delta T}{R_{\text{th-total}}}$$

Conclusion:

Even with an ideal heat sink ($R_{\text{th-heatsink}} = 0$) we cannot dissipate the required 5W. In this case we need an LED with less thermal resistance.



Practical Example

We need 1W for our light output

We have again:

$$T_{\text{junction}} = 120 \text{ }^\circ\text{C}$$

$$T_{\text{ambient}} = 40 \text{ }^\circ\text{C}$$

$$R_{\text{th-LED}} + R_{\text{th-MCPCB}} + R_{\text{th-TIM}} = 17.5 \text{ K/W}; R_{\text{th-heatsink}} = ?$$

Which heat sink is OK?

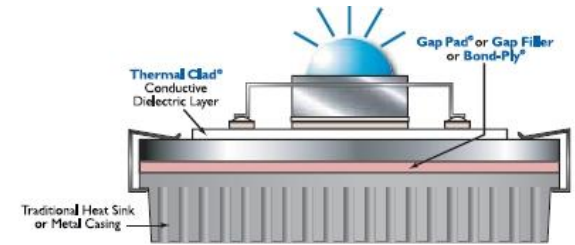
$$q = 80 / (17.5 + R_{\text{th-heatsink}}) ; R_{\text{th-heatsink}} = 62.5 \text{ K/W}$$

We found earlier:

$$A=20 \text{ cm}^2, h=10 \text{ W/m}^2\text{K} \rightarrow R_{\text{th-heatsink}} = 50 \text{ K/W}$$

Conclusion:

We can use a simple heat sink with natural convection.

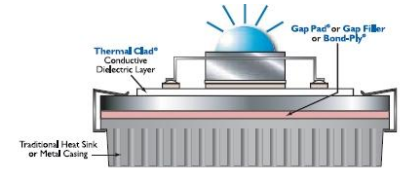


$$q = \frac{\Delta T}{R_{\text{th-total}}}$$



Practical Example Conclusion

Thermal resistance of the MCPCB does not play any role



- In our first case, the LED thermal resistance was dominant; while in the last case, the convective resistance was dominant.
- Hence, *from a thermal point only*, you can choose MCPCBs with a much lower thermal performance and, hence, lower cost.
- The thermal performance of the PCB is relevant only for very high heat flux cases (e.g. liquid cooling) and for top-of-the-bill LEDs.



Nomenclature

The confusing situation regarding *'thermal impedance'*

Fact:

'Electrical impedance' is historically reserved to describe time-dependent electrical resistance. In the limit of steady state, thermal impedance equals thermal resistance → hence, units should be the same!

Hence,

'Thermal impedance', as used by U.S. vendors, violates the electro-thermal analogy, because:

- Unit does not correspond (K/W vs. m^2K/W)
- Definition does not correspond (time-dependent vs. steady state)

Is this a problem?

Yes, because time-dependent (dynamic) test methods will be increasingly used, one output of which is the *'correct'* thermal impedance.

Proposal:

Use thermal resistance per unit area, or unit R_{th} .



Electrical Properties

Presented by Michael Gay (Isola) and Norm Berry (Insulectro)



Common Tests

- **Insulation Resistance (IR)**
 - This test is used to provide a quantifiable resistance value for all of a product's insulation
- **Dielectric Breakdown Strength Test**
 - The test voltage is increased until the dielectric fails, or breaks down, allowing too much current to flow.
- **Dielectric Withstand Voltage Test (DWS) or High Potential Test (HiPot)**
 - A standard test voltage is applied (below the established Breakdown Voltage) and the resulting leakage current is monitored
- **Conductive Anodic Filament Test (CAF)**
 - This test is used to determine the capability of the material for various design feature spacing under high humidity conditions with applied voltage



Typical Proof Test (VDC)

Proof Test or High Potential Test (HiPot)

A standard non-destructive test voltage is applied (below the established Breakdown voltage) and the resulting leakage current is monitored. The test is done to evaluate the integrity of the dielectric material.



SATURN ELECTRONICS
CORPORATION

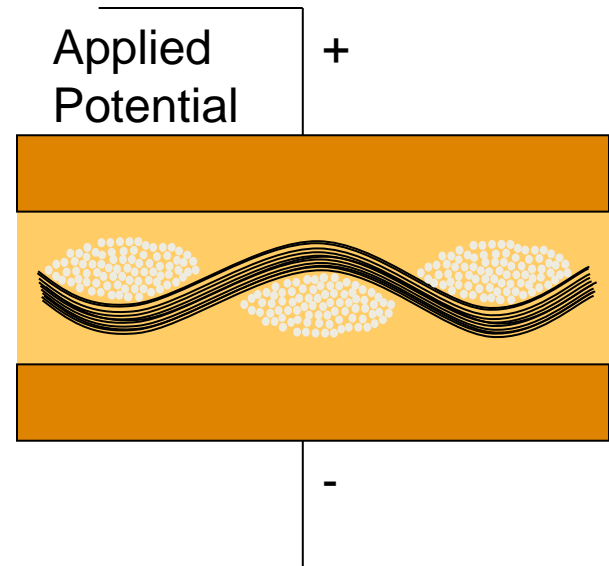
Typical Proof Test (VDC)

High Potential Dielectric Testing (HiPot)

This non-destructive testing methodology is used to characterize the laminate material insulation capability under a specified potential. Leakage current is measured and compared to predetermined limits

Typical Test Conditions:

- 500-2500 Volts DC (VDC)
- 700-1200 Volts AC @50-60 Hz (VAC)
- Up to 30 seconds
- 10 M Ω – 500 M Ω
- 10 μ A – 100 μ A





SATURN ELECTRONICS
CORPORATION

Breakdown (kV AC)

Breakdown Voltage Test

Breakdown voltage is the stress at failure when AC at power frequency is applied using a rate of rise is 500 Volts/second. Breakdown voltage testing does not relate to proof stress “Proof Testing”.

Breakdown voltage is the potential difference at which **dielectric failure** occurs under prescribed conditions in an electrical insulating material located between two electrodes.



SATURN ELECTRONICS
CORPORATION

Breakdown (kV AC)

Dielectric Breakdown Voltage

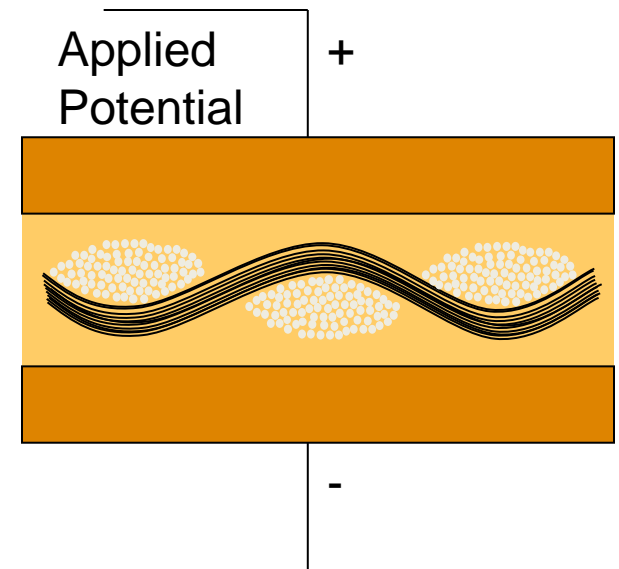
This testing methodology is used to characterize the laminate material insulation capability to failure.

Typical Test Conditions:

Ramp Volts AC @50-60 Hz (VAC) until failure

Example:

Determine the electric strength in volts per mil for each specimen by dividing the breakdown voltage expressed in kilovolts by the thickness express in inches.



$$ES = (6.8 \text{ KV} / .005 \text{ inch}) \times (1000 \text{ V} / \text{KV}) \times (1 \text{ inch} / 1000 \text{ mils}) = 1360 \text{ v/mil}$$



SATURN ELECTRONICS
CORPORATION

Permittivity (Dk)

Typical thermal management materials are modified to have higher thermal conductivity. The modifications of the dielectric material raise the Dk of the material to the range of 6 or higher.



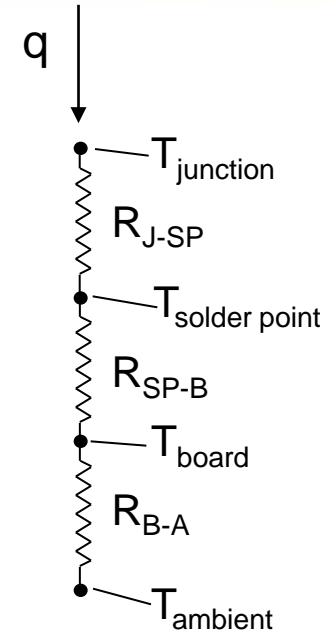
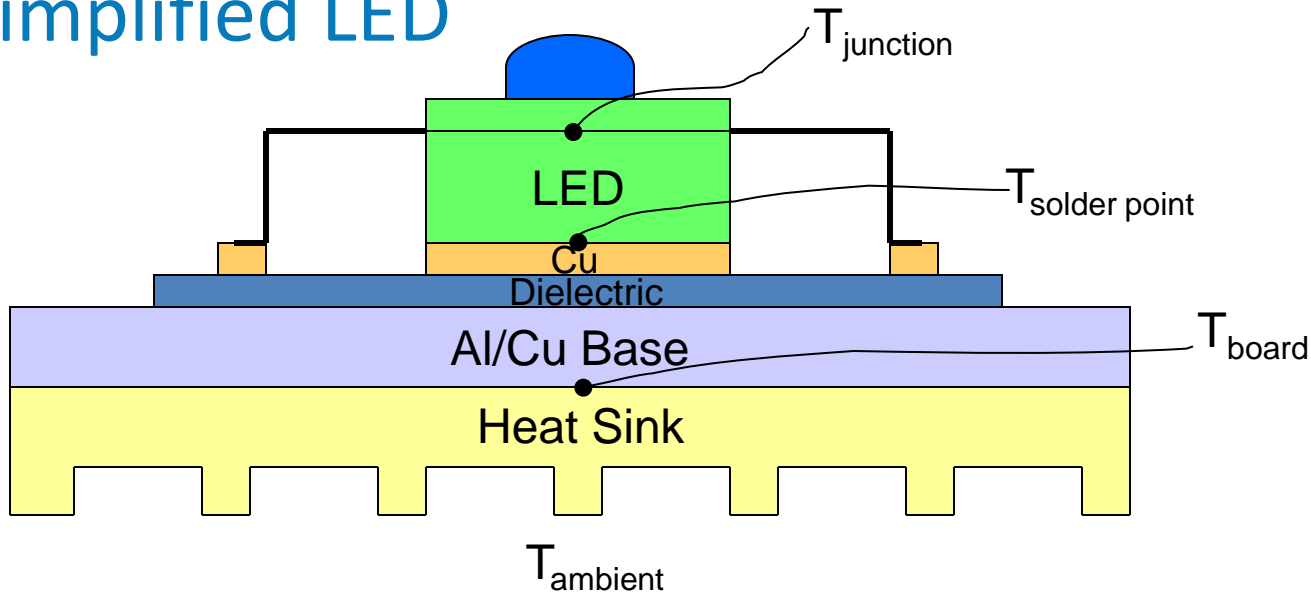
SATURN ELECTRONICS
CORPORATION

Product Reliability

Presented by Richard A. Wessel of DuPont



Simplified LED



Big concern: what is $T_{junction}$?

Why?

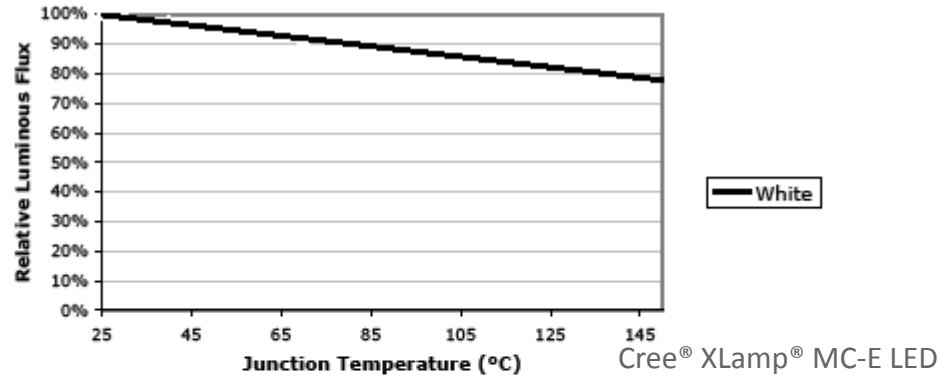


Lower T_{junction} Better

Increased relative luminous flux for lower junction or thermal pad temperature

Relative Flux vs Junction Temperature ($I_f = 350 \text{ mA}$)

The following graph represents typical performance of XLamp MC-E LEDs with all four LEDs driven in series at 350 mA.



Luxeon®
Rebel

Red, Red-Orange and Amber at Test Current

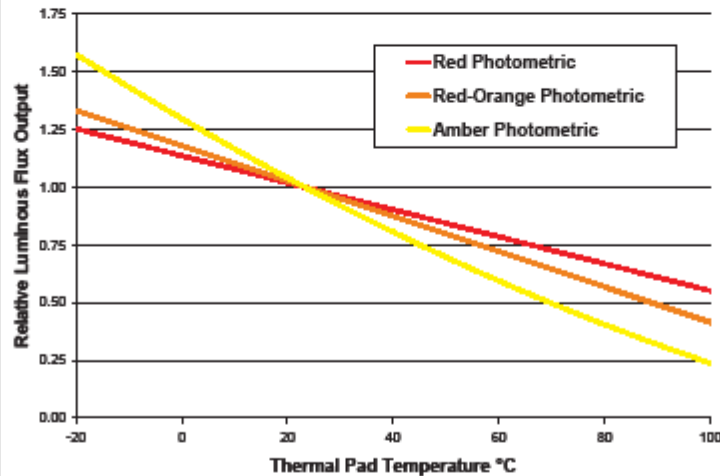


Figure 7. Relative light output vs. Thermal Pad temperature for Red, Red-Orange and Amber.

Cool-White, Neutral-White, Warm-White, Green, Cyan, Blue and Royal-Blue at Test Current

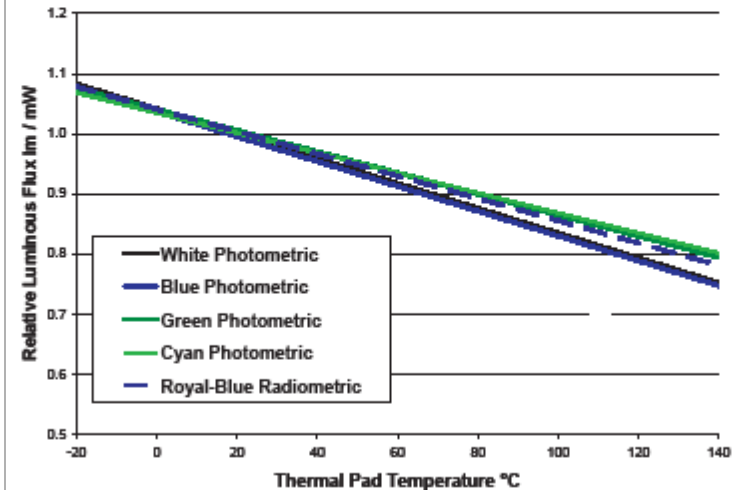


Figure 8. Relative light output vs. Thermal Pad temperature for White, Green, Cyan, Blue and Royal-Blue.

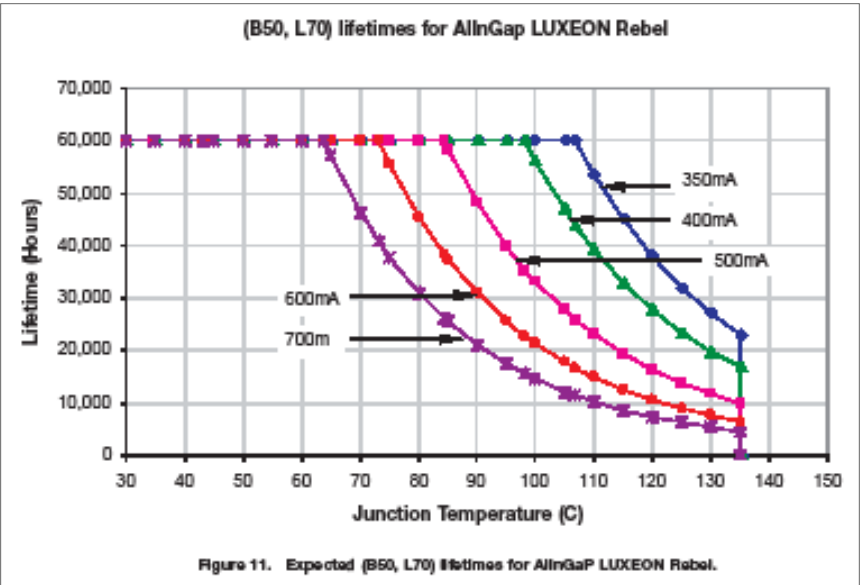
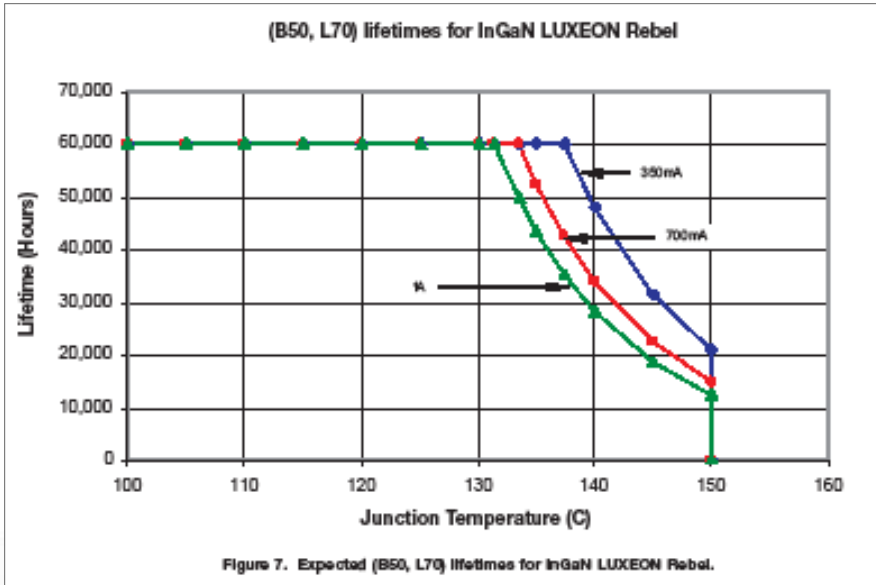


Increased Lifetimes

Lower Junction Temperature

Increased lifetimes for lower junction temperature

Luxeon® Rebel





Suggested Fabrication Notes

Taking Control of Your Design!



Suggested Fabrication Notes

Purpose of Fab Notes

Take ***your*** requirements for each characteristic that ***you*** deem most important and specify (values for thermal conductivity and electrical insulation resistance).

We also suggest including a list of pre-approved materials.



Suggested Fabrication Notes (cont.)

Example of a Fab Note

Copper Weight: 2 oz.

Metal Core: 0.060" Al 5051

Dielectric:

Thermal Conductivity: Must meet or exceed 1.3 ($^{\circ}\text{W}/\text{m}\cdot\text{K}$)

Thermal Resistance: Maximum 0.9 ($^{\circ}\text{C in}^2/\text{W}$)

Electrical Insulation: Must meet or exceed 2,000 VDC

Any other characteristic you feel is important: XYZ

Currently Approved Materials:

- Bergquist HT-07006
- Bergquist LTI-06005
- Laird T-lam SS 1KA06
- DuPont Coolam



SATURN ELECTRONICS
CORPORATION

Suggested Fabrication Notes (cont.)

Benefits of Fab Notes

Allows supplier to quote *multiple vendors*.

Subsequent Results

- Lower Cost
- Quicker Lead Times
- Adaptability to take advantage of new technologies down the road
- Introduce competition from the raw materials and finished PCB suppliers



Materials Chart

Thermal Dielectric Material Selection Chart

Brand		Thermal Characteristics		Dielectric Characteristics / Insulation			Other		
Material Manufacturer	Material Type	Resistance (°C in ² /W)	Conductivity (°W/m-K)	Typical Proof Test (VDC)	Breakdown (kVAC)	Permittivity (Dk)	Glass Trans (°C)	UL Index (°C)	Peel Strength (lb/in)
Bergquist	HT-04503	0.05	2.2	1500	6.0	7	150	140 / 140	6
Bergquist	HT-07006	0.07	2.2	2500	11.0	7	150	140 / 140	6
Bergquist	LTI-04503	0.05	2.2	1500	6.5	7	90	130 / 130	6
Bergquist	LTI-06005	0.09	2.2	2000	9.5	7	90	130 / 130	6
Bergquist	MP-06503	0.09	1.3	1500	8.5	6	90	130 / 140	9
Bergquist	CML-11006	0.21	1.1	2500	10.0	7	90	130 / 130	10
Laird	T-lam SS 1KA04	0.05	3	1200		4.3 / 4.1	105	110	4.5
Laird	T-lam SS 1KA06	0.08	3	2500		4.3 / 4.1	105	120	4.5
Laird	T-lam SS 1KA08	0.11	3	3500		4.3 / 4.1	105	130	5
Laird	T-lam SS HTD04	0.072	2.2	4000+	2.5	5.1 / 4.9	168	150	6.5
Laird	T-lam SS HTD06	0.107	2.2	6000+	3.5	4.9 / 4.7	168	150	7
ISI	Zeta Bond 1.0 mil						> 300°		
ISI	Zeta Bond 1.5 mil			1000			> 300°		
DuPont Coolam	LX03517016	0.05	0.8	2500		5.5	225	130	14
DuPont Coolam	LX07022016	0.065	0.8	4000		5.5	225	130	14
UniPlus	UP-HTC-P075016	0.09	1.3	1500	8.3	4.8	135	140 / 110	9.5
Iteq	IT-858T (80 um)	0.128	2.2	> 6000	>4.0		159		
Iteq	IT-858T (100 um)	0.128	2.2	> 6000	>4.0		159		
Iteq	IT-859GT (80 um)	0.126	2.2	> 6000	>4.0		156		
Iteq	IT-859GT (100 um)	0.126	2.2	> 6000	>4.0		156		
Taconic	TacLED-4	0.19	0.4	> 3000	>3.0	3.05	327		12
Taconic	TacLED-10	0.13	1		>6.0	4.6	136		9.5
Taconic	TacLED-20	0.06	2		>6.0	5.2	125		8.4



SATURN ELECTRONICS
CORPORATION

Part Two

Non-browning White Soldermask





SATURN ELECTRONICS
CORPORATION

White Soldermask

Current Resin Systems

- Focus on initial thermal shock, not constant heat
- Tend to Brown over time
- Not developed to be a Reflecting Surface for LEDs



SATURN ELECTRONICS

C O R P O R A T I O N

White Soldermask (cont.)

Desired Resin Systems

- Remain white through Assembly and Lifespan of LED final product
- Have high reflectivity to enhance LED performance
 - Some believe high reflection soldermask results in lower power consumption for same light output



What are the Solutions?

New White High Temperature Liquid Photo-Imageable Soldermasks

- Past two years a number of “LED” white soldermasks have been introduced
 - Unfortunately we have not seen improvements in all of them
- Through numerous studies we have so far found two offerings that show significant improvement:
 - Peters (***SD2491SM TSW***)
 - Sun Chemicals (***CAWN 2589/2591***)



What are the Solutions? (cont.)

New White High Temperature Thermal Soldermasks

If *Bright* white soldermask is the objective, these solutions may not suffice

- Suggest base coat of LPI White then topcoat of High-Temp thermal white soldermask
- After numerous thermal whites, one does not brown after multiple cycles (*Peters SD2496TSW*)
- This is the formula behind “proprietary” white soldermasks offered by other PCB vendors



Cost Expanders

New White High Temperature Liquid Photo-Imageable Soldermasks

- To date, we've seen cost increases over standard soldermask price of 30% - 100%
 - Approximately .20 to .30 cents per panel (18" x 24")

New White High Temperature Thermal Soldermasks

- To date, we've seen cost increases over standard soldermask price of > 100%
 - Approximately \$1 per panel (18" x 24")
 - Includes labor and set up for secondary application process



Thermal Webinar Conclusion

SPECIFY your needs for thermal performance of the dielectric

SPECIFY your needs for the electrical performance of the dielectric

SPECIFY your needs in context of entire product, not just PCB (when applicable)

KNOW that you have white soldermask choices

but keep your fab notes open to take advantage of future developments

PCB Flow Chart

